

ENSC327

Communications Systems

12: FM Demodulation: Frequency Discriminator



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Three FM Demodulation Methods

- ❑ Frequency discriminator (slope detector)
 - Balanced freq. discriminator
- ❑ Phase-locked loop (PLL) demodulator
- ❑ Quadrature detector (not covered in this course, but is used in our lab equipment, see Lab 4)

Overview of FM Demodulation

FM signals:

$$s(t) = A_c \cos(2\pi f_c t + 2\pi k_f \int_0^t m(\tau) d\tau)$$

- To recover the message $m(t)$:
 - Need a circuit whose output is proportional to the difference of the instantaneous frequency from the carrier frequency:

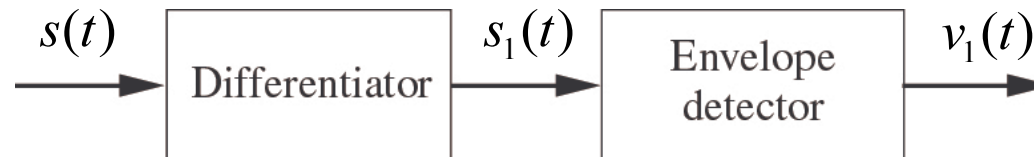
- Two methods:
 - Frequency discriminator (slope detector)
 - Phase locked loop

Ideal Freq. Discriminator

$$s(t) = A_c \cos(2\pi f_c t + 2\pi k_f \int_0^t m(\tau) d\tau)$$

□ If we take the **derivative** of $s(t)$:

Ideal Freq. Discriminator

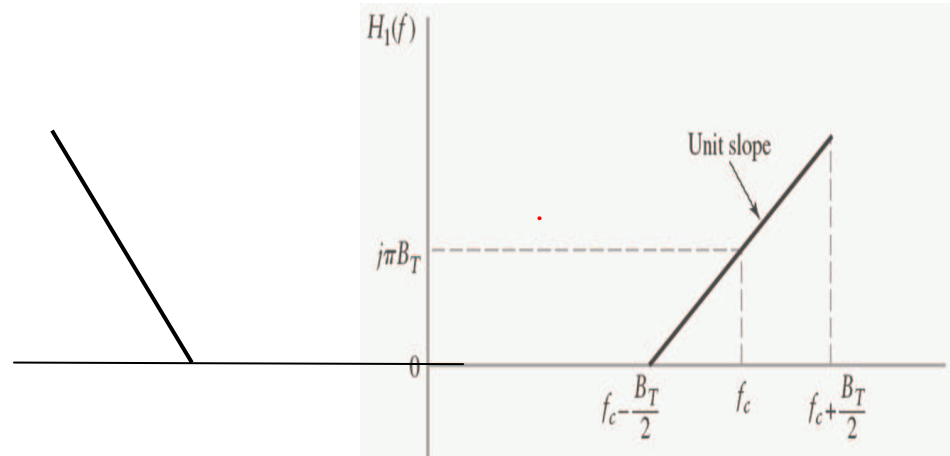


- Recall: Freq response of the differentiator:

- ➔ The differentiation operator corresponds to a filter
 - Problem:
 - Practical implementation:

Practical Freq. Discriminator

- Freq response of the differentiator (for $f > 0$):
- $H_1(f)$ for $f < 0$ is defined by using conj. symmetry.



- To find the output of this filter for the input $s(t)$:

$$s(t) = A_c \cos(2\pi f_c t + 2\pi k_f \int_0^t m(\tau) d\tau)$$

Practical Freq. Discriminator

- We first find the complex envelope of $s(t)$:

- We next find the complex envelope of the differentiator :

$$\text{From } H_1(f) = \begin{cases} j2\pi(f - (f_c - B_T / 2)), & f_c - B_T / 2 \leq f \leq f_c + B_T / 2, \\ 0, & \text{otherwise} \end{cases}$$

Practical Freq. Discriminator

□ complex envelope:

Note: Eq. (4.49) should be doubled, as in Eq. (3.44).

As a result, Eqs. (4.50) to (4.55) should be doubled too.

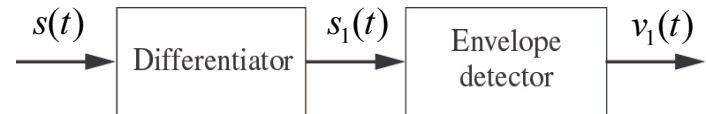
□ The complex envelope of the output is: $\tilde{s}(t) \rightarrow \boxed{\tilde{h}_1(t)} \rightarrow 2\tilde{s}_1(t)$

Practical Freq. Discriminator

- Taking inverse FT:

Practical Freq. Discriminator

$$\tilde{s}_1(t) = j\pi A_c B_T \left[1 + \frac{2k_f}{B_T} m(t) \right] e^{j2\pi k_f \int_0^t m(\tau) d\tau}$$



□ From $\tilde{s}_1(t)$ we can find $s_1(t)$:

Practical Freq. Discriminator

□ How to remove the bias in $v_1(t) = \pi A_c B_T \left[1 + \frac{2k_f}{B_T} m(t) \right]$?

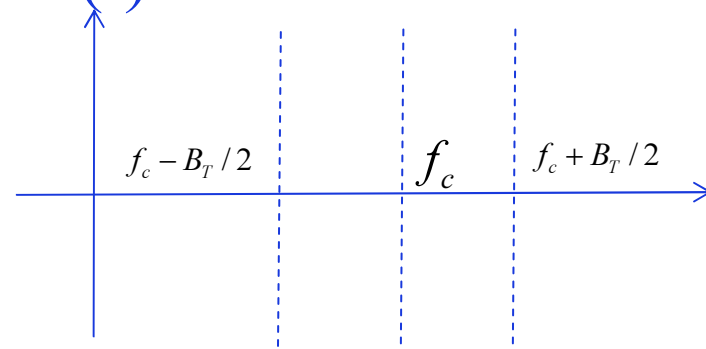
□ If we can get another signal: $v_2(t) = \pi A_c B_T \left[1 - \frac{2k_f}{B_T} m(t) \right]$

Then the bias can be cancelled by:

□ This requires another filter for $v_2(t)$:

$$H_2(f) = j2\pi(f - (f_c + B_T / 2)),$$

for $f_c - B_T / 2 \leq f \leq f_c + B_T / 2$,



Practical Freq. Discriminator

□ To verify:

$$H_2(f) = j2\pi(f - (f_c + B_T / 2)), \text{ for } f_c - B_T / 2 \leq f \leq f_c + B_T / 2,$$

□ Taking inverse FT:

Practical Freq. Discriminator

$$\tilde{s}_2(t) = j\pi A_c B_T \left[-1 + \frac{2k_f}{B_T} m(t) \right] e^{j2\pi k_f \int_0^t m(\tau) d\tau} \quad \Rightarrow$$

Practical Freq. Discriminator

- The previous derivation means that we need the following circuit, which is called **balanced** frequency discriminator:

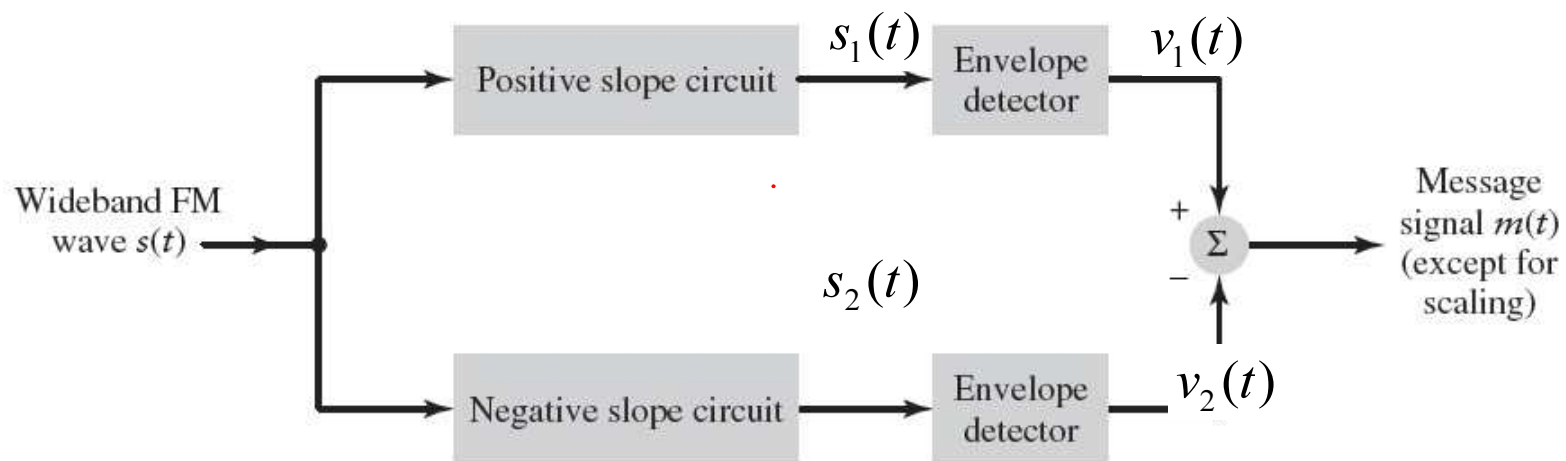


FIGURE 4.13 Block diagram of balanced frequency discriminator.